

# Optical properties of As<sub>2</sub>S<sub>3</sub>-based suspended-core photonic crystal fiber

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**Abstract.** In this paper, the nonlinear properties of photonic crystal fibers (PCF) with As<sub>2</sub>S<sub>3</sub> substrate were analyzed numerically. With the suspended-core design, we achieve an anomalous dispersion regime with one or two zero-dispersion wavelengths, which is flat and has a small value at the investigated wavelength. The high nonlinear coefficient and very low confinement loss in the wavelength range of 1–3 μm, in comparison with other publications, are the outstanding advantages of these suspended-core PCFs. The highest nonlinear coefficient (28,527.374 W<sup>-1</sup>.km<sup>-1</sup>), smallest effective mode area (0.593 μm<sup>2</sup>), and low confinement loss (6.050 × 10<sup>-17</sup> dB.m<sup>-1</sup>) at the wavelength of 1.55 μm were observed in the PCFs with a fiber diameter of 16.07 μm. Based on the numerical simulation results, we proposed two optimal structures suitable for supercontinuum generation.

**Keywords:** suspended-core PCF, flat dispersion, high nonlinear coefficient, low loss, supercontinuum generation

## 1 Introduction

Photonic crystal fiber (PCF) is a special type of optical waveguide based on photonic crystals, published in the 90s of the last century, and it attracted the attention of different research groups [1]. In recent years, the excellent propagation properties of PCFs, including linear and nonlinear parameters, have been investigated and controlled as desired [2-4]. Photonic crystal fibers have numerous applications in science and engineering [5-9] because of their outstanding optical properties. The PCF's design versatility via adjusting their lattice parameters to achieve exceptional optical properties, such as endlessly monomodal propagation, high nonlinearity, low confinement loss, and tunable chromatic dispersion profile, allow PCFs to be an excellent nonlinear medium to enhance supercontinuum (SC) generation performance [10-16]. In most studies on SC generation via PCFs, silica has been

used as a common background material. However, the operating wavelength range is limited because of its high matter loss above the 2 μm wavelength, so it is difficult to generate SC in the infrared region. As a result, non-silica, such as chalcogenide glass, has great advantages in investigating nonlinear optical effects in PCFs because of the high nonlinearity of chalcogenide glasses in comparison with other glasses. This opens up the possibility of achieving interesting nonlinear properties in the longer wavelength range.

To improve the spectral range of SC light, researchers have already presented various designs, including selectively changing their cladding geometries, selecting a substrate material with a high nonlinear coefficient, or both to control the nonlinear properties of PCFs. In 2001, a new design of a microstructured optical fiber called "suspended-core fiber" was suggested

by Monro et al. [17], with the preform geometry consisting of three holes centred on a central solid core. Then, Kiang et al. [18] reported a suspended-core fiber with lead-silicate glass in 2002. Kumar et al. and Petropoulos et al. [19, 20] also described a suspended-core fiber with tellurite and lead-silica glasses in 2003. Since then, suspended-core fiber has become a relatively new class of fibers and a subclass of microstructured fibers. The fiber microstructure consists of a triangular lattice of air holes that extend along the fiber. They surround a tiny central core with triangle geometry attached to a robust jacket with three thin struts [21].

The choice of high nonlinearity substrate material such as  $\text{As}_2\text{S}_3$  is also an excellent solution to further improve the SC generation efficiency and achieve a broader, smoother, and better coherence SC spectrum. In 2013, Gao et al. [22] reported an  $\text{As}_2\text{S}_3$  suspended-core fiber with a core diameter of  $3.2 \mu\text{m}$ . Its nonlinear coefficient and the effective mode area at the  $2.5\text{-}\mu\text{m}$  wavelength were  $894.2 \text{ W}^{-1}\cdot\text{km}^{-1}$  and  $8.43 \mu\text{m}^2$ . The SC generation process with a flat dispersion and zero-dispersion wavelengths (ZDWs) of  $2.52 \mu\text{m}$  is investigated in detail. A chalcogenide ( $\text{As}_2\text{S}_3$ )-based ridge waveguide with a suspended structure on  $\text{Si}_3\text{N}_4$  substrate was designed by Jing et al. [23] in 2018, which had low and flat dispersion profiles. Also, in 2018, the nonlinear coefficient and effective mode area of  $561 \text{ W}^{-1}\cdot\text{km}^{-1}$  and  $18.4 \mu\text{m}^2$  at the  $2\text{-}\mu\text{m}$  wavelength were achieved in an  $\text{As}_2\text{S}_3$  suspended-core fiber with four holes fabricated by Si et al. [24]. Furthermore, the dispersion curve was relatively flat with a maximum of  $14.19 \text{ ps}\cdot\text{nm}^{-1}\cdot\text{km}^{-1}$  at the  $3\text{-}\mu\text{m}$  wavelength, and double zero-dispersion wavelengths in the infrared region were  $2.59$  and  $3.63 \mu\text{m}$ .

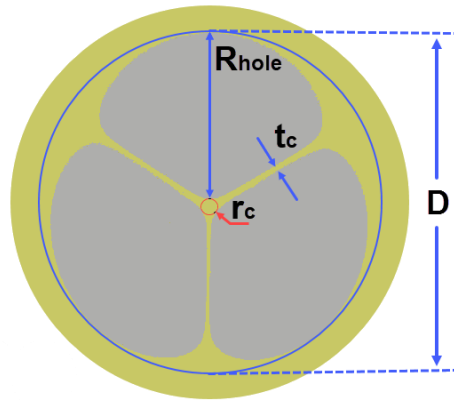
Although these works achieved small and flat dispersions, they were beneficial for generating SC with a low nonlinear coefficient, a

large effective mode area, and high loss. Simultaneous optimization of the optical properties of PCFs is an essential factor in improving SC generation efficiency, so many research groups have been focusing on this goal.

In this work, we selected an  $\text{As}_2\text{S}_3$  composition glass, one of the types of chalcogenide glasses, as a promising material because of its high nonlinearity (100–500 times that of silica glass), low intrinsic loss of the material ( $0.01\text{--}0.1 \text{ dB}\cdot\text{km}^{-1}$ ), and potential to tailor dispersion [25]. The PCFs were designed with a suspended-core structure consisting of three air holes with various lattice parameters. Their optical properties were simulated and investigated in detail. The flat dispersion characteristics, high nonlinear coefficients, and very low confinement loss are the outstanding advantages of these PCFs.

## 2 Numerical modelling of PCFs

The Lumerical Mode Solutions software was used to design the structure and determine the modal properties of fibers. This software supports several higher-order modes apart from the fundamental mode. The arsenic trisulfide ( $\text{As}_2\text{S}_3$ ) PCF used in this simulation has a suspended-core structure with three holes. Its cross-section geometrical structure is shown in Fig. 1a. The light propagates in the defect of the fiber structure. To increase modal nonlinearity and optimize PCF structures, we designed PCFs with various lattice parameters, such as the radius of air holes,  $R_{\text{hole}}$ , the radius of the core,  $r_c$  (which was defined as the radius of the circle inscribed in the triangular core), the thickness of  $\text{As}_2\text{S}_3$  bridge,  $t_c$ , and the diameter of the fiber,  $D$ . Fig. 1b shows that the light is strongly confined to the core of PCFs when  $R_{\text{hole}} = 7.615 \mu\text{m}$ ;  $r_c = 0.41 \mu\text{m}$ ;  $t_c = 0.125 \mu\text{m}$ , and  $D = 16.070 \mu\text{m}$ .



(a) ■ Air ■ Arsenic trisulfide

Fig. 1a. Cross-section geometrical structure of PCF with suspended core

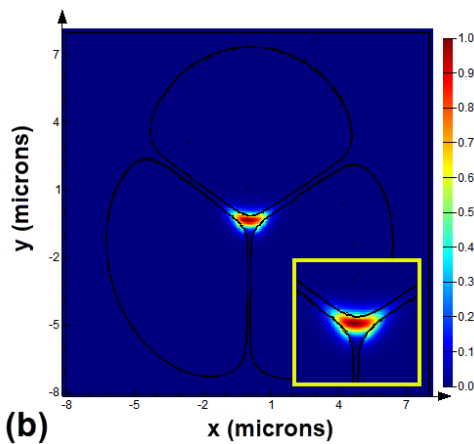


Fig. 1b. Light confined in core of PCF when  $D = 16.07 \mu\text{m}$

With the  $\text{As}_2\text{S}_3$  glasses, the refractive index as a function of wavelength is given in the four-term Sellmeier equation as [2]:

$$n^2 = 1 + \frac{1.9\lambda^2}{\lambda^2 - 0.022^2} + \frac{1.92\lambda^2}{\lambda^2 - 0.062^2} + \frac{0.87\lambda^2}{\lambda^2 - 0.122^2} \quad (1)$$

The numerical simulations were conducted for the PCFs with  $D$  changing from 16.07 to 64.28  $\mu\text{m}$  by using the finite difference eigenmode (FDE) method. The process of FDE utilizes the Maxwell wave equation. The boundary condition is the perfectly matched layers to analyze the structure which makes no reflection at the boundary and reduces the loss. In addition, the fiber cross-section is divided into many

rectangular sections to reduce meshing errors and increase the numerical accuracy of the simulations.

### 3 Optical properties of PCFs

#### 3.1 Effective refractive index

The real part of the effective refractive indices corresponding to the fundamental mode over the wavelength range from 1 to 3  $\mu\text{m}$  was found and shown in Fig. 2.

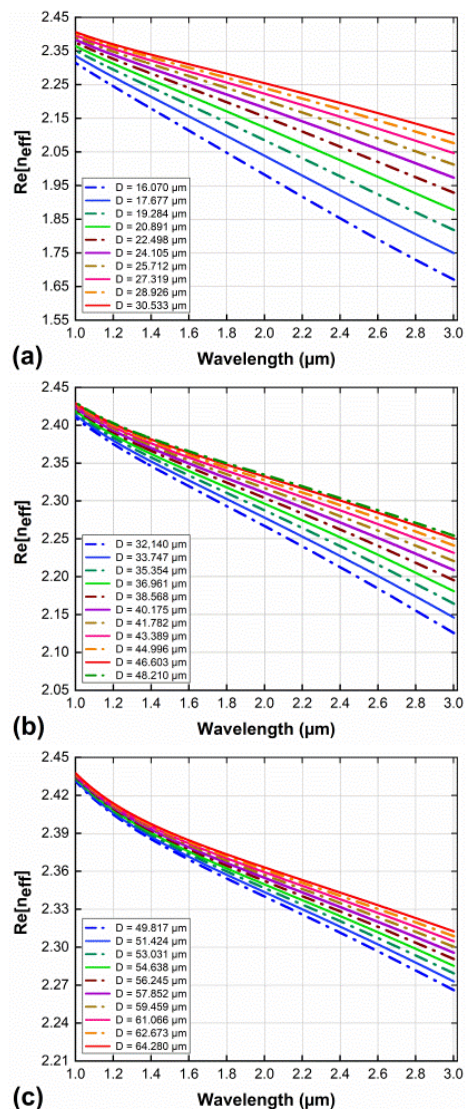


Fig. 2. Real part of effective refractive index as function of wavelength with various fiber diameters

For all cases, the real part of the effective refractive index ( $\text{Re}[n_{\text{eff}}]$ ) decreases monotonically when the wavelength increases because of the stronger penetration of long wavelengths into the cladding region of PCFs. A change in the diameter of the fiber ( $D$ ) strongly affects the  $\text{Re}[n_{\text{eff}}]$ ; an increase in  $D$  causes the  $\text{Re}[n_{\text{eff}}]$  to increase. The refractive index of the medium's material varies when an intense input pulse propagates through the nonlinear medium, which causes the effective refraction index to change as well. The light interaction ability in the nonlinear

medium of small-core PCFs is stronger than of the large-core PCFs, so the real part of the effective refraction index is larger in the case of a larger core.

The value of the real part of the effective refraction index of PCFs with various  $D$  is calculated at the 1.55  $\mu\text{m}$  wavelength and displayed in Table 1. The maximum and minimum values of  $\text{Re}[n_{\text{eff}}]$  are 2.388 and 2.13 when  $D = 64.280$  and 16.070  $\mu\text{m}$ . The small difference between the two refractive index values for both cases is 0.258.

**Table 1.** Real part of effective refractive index at 1.55  $\mu\text{m}$  wavelength of PCFs with various fiber diameters

| $D$ ( $\mu\text{m}$ ) | $\text{Re}[n_{\text{eff}}]$ | $D$ ( $\mu\text{m}$ ) | $\text{Re}[n_{\text{eff}}]$ | $D$ ( $\mu\text{m}$ ) | $\text{Re}[n_{\text{eff}}]$ |
|-----------------------|-----------------------------|-----------------------|-----------------------------|-----------------------|-----------------------------|
| 16.070                | 2.130                       | 32,140                | 2.326                       | 48.210                | 2.37                        |
| 17.677                | 2.171                       | 33.747                | 2.333                       | 49.817                | 2.373                       |
| 19.284                | 2.203                       | 35.354                | 2.340                       | 51.424                | 2.375                       |
| 20.891                | 2.230                       | 36.961                | 2.345                       | 53.031                | 2.377                       |
| 22.498                | 2.251                       | 38.568                | 2.350                       | 54.638                | 2.379                       |
| 24.105                | 2.269                       | 40.175                | 2.354                       | 56.245                | 2.381                       |
| 25.712                | 2.284                       | 41.782                | 2.358                       | 57.852                | 2.382                       |
| 27.319                | 2.297                       | 43.389                | 2.362                       | 59.459                | 2.384                       |
| 28.926                | 2.308                       | 44.996                | 2.365                       | 61.066                | 2.385                       |
| 30.533                | 2.318                       | 46.603                | 2.368                       | 62.673                | 2.386                       |
|                       |                             |                       |                             | 64.280                | 2.388                       |

### 3.2 Chromatic dispersion

We numerically calculated the chromatic dispersion coefficient of the PCFs, including both waveguide and materials dispersion by using the real part of the effective index according to the following formula

$$D_c = -\frac{\lambda}{c} \frac{d^2 \text{Re}[n_{\text{eff}}]}{d\lambda^2} \quad (2)$$

where  $\text{Re}[n_{\text{eff}}]$  is the real part of  $n_{\text{eff}}$ , which is the effective index of a guided mode calculated by means the FDE method, and  $c$  is the velocity of light in the vacuum.

Fig. 3 illustrates the dispersion profiles of PCFs in terms of wavelength. As can be observed in this figure, the PCFs exhibit anomalous dispersion with a larger shift of zero-dispersion wavelengths towards the longer wavelength region as the fiber diameter increases. The large core fibers with a fiber diameter greater than 24.105  $\mu\text{m}$  have anomalous dispersion with one ZDW. Meanwhile, anomalous dispersion with double ZDWs is observed in fibers with a smaller diameter. The zero-dispersion wavelength

(ZDW<sub>1</sub>) is located around 1.45–1.65  $\mu\text{m}$ , and the other (ZDW<sub>2</sub>) is from 1.83 to 2.84  $\mu\text{m}$ . The two ZDWs divide the entire spectrum into three dispersion regions, i.e., a region with abnormal dispersion sandwiched between two regions with normal dispersion. Compared with a PCF with one ZDW, the soliton self-frequency shift has a clear redshift boundary that is close to the second ZDW [26]. The presence of a negative dispersion slope near the second ZDW causes a redshift in dispersive waves [27] in the second normal dispersion region and the trapped wave [28] because of phase matching between the redshifted soliton and the redshifted dispersive waves. The former effect broadens the supercontinuum to the red end, while the latter flattens the supercontinuum lying between redshift soliton and redshifted dispersive waves. For instance, an enhanced SC bandwidth with improved flatness was demonstrated in PCFs by generating two dispersive waves in the short- and long-wavelength sides of the SC spectrum [29]. Obviously, by carefully selecting the geometry of the structure and changing the lattice parameters in the simulation, we achieved anomalous dispersion with double ZDWs, similar to that of Si et al. [24], but it was not observed in other works [22, 23]. The anomalous dispersion with two ZDWs is one of the outstanding advantages of this work, suitable for some SC generations with the influence of soliton-induced effects.

### 3.3 Effective nonlinearity

The nonlinear coefficient is one of the parameters that govern the SC spectral width because of the interaction of the input pulse with the nonlinear optical medium. To extend the SC spectrum further, we need the nonlinear coefficient as high as possible. The nonlinear coefficient ( $\gamma$ ) is a measure of the nonlinearity of the medium, and it can be estimated according to Formula 3 [30].

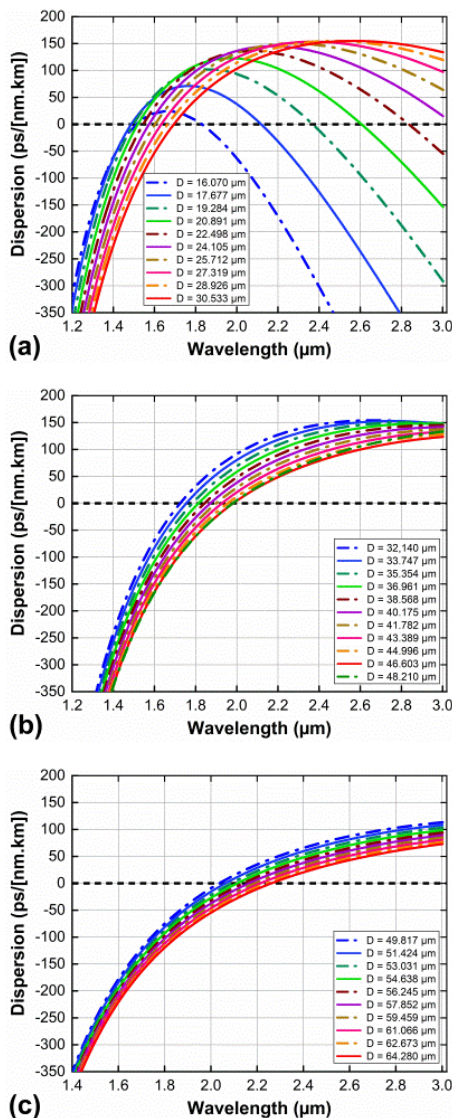


Fig. 3. Chromatic dispersion of PCFs with various fiber diameter

$$\gamma(\lambda) = 2\pi \frac{n_2}{\lambda A_{\text{eff}}} \quad (3)$$

where  $A_{\text{eff}}$  is the effective mode area for the basic mode of the fiber and  $n_2$  is the nonlinear refractive index of the optical material ( $4.21 \times 10^{-18} \text{ m}^2 \cdot \text{W}^{-1}$  at  $1.55 \text{ }\mu\text{m}$ ) for  $\text{As}_2\text{S}_3$  [31]. The effective mode area for the fundamental mode can be calculated according to Formula 4 [30], where  $E$  is the transverse electric field over the cross-section of the PCF

$$A_{\text{eff}} = \frac{\left( \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} |E|^2 dx dy \right)^2}{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} |E|^4 dx dy} \quad (4)$$

Using a material with a high nonlinear refractive index, such as  $\text{As}_2\text{S}_3$ , or paying attention to structural designs of PCFs for a smaller

effective mode area ( $A_{\text{eff}}$ ), or by a combination of both ways, can increase the value of the nonlinear coefficient. The variation of the nonlinear coefficient and the effective mode area as functions of wavelength is presented in Figs. 4 and 5.

The nonlinear coefficient has a large value (tens of thousands of  $\text{W}^{-1} \cdot \text{km}^{-1}$ ) at short wavelengths and decreases with increasing wavelength. The light is no longer confined strongly inside the core of PCFs in the long-wavelength range because the modes get leaked through the holes and in between them, increasing the effective mode area. A small effective area is often observed in small-core fibers due to the strongly confined light in the core. This causes the nonlinear coefficient to decrease as the fiber diameter increases in the studied wavelength region.

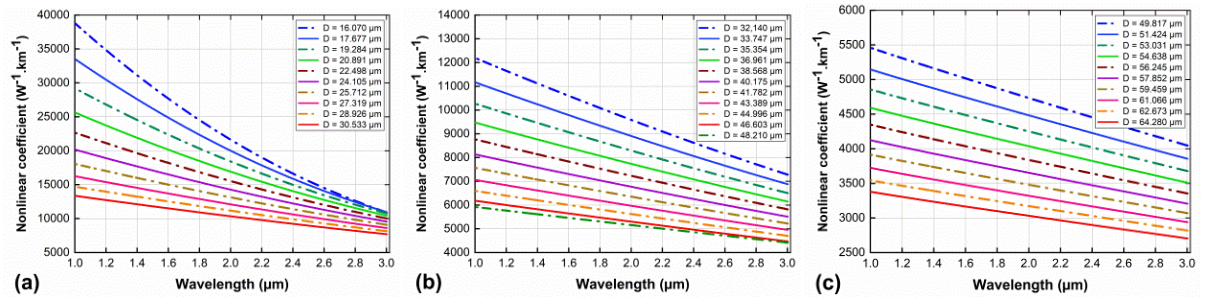


Fig. 4. Nonlinear coefficient of PCFs with various fiber diameter

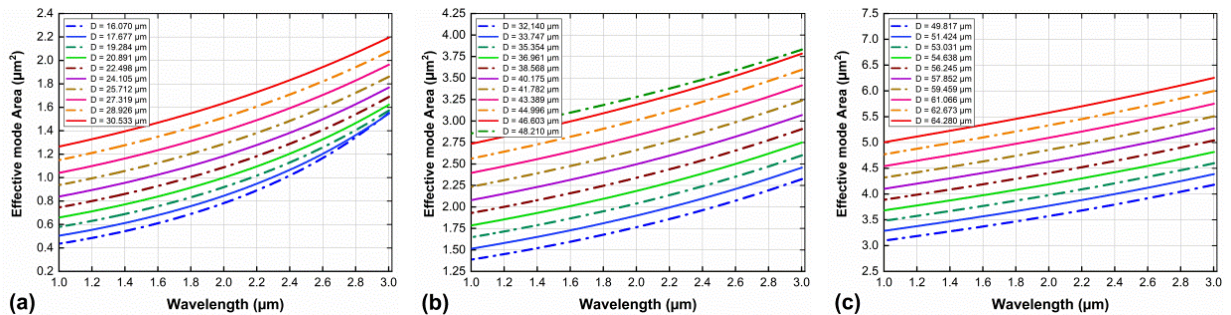


Fig. 5. Effective mode area of PCFs with various fiber diameter

The values of the nonlinear coefficients and the effective mode area at the 1.55  $\mu\text{m}$  wavelength are presented in Tables 2 and 3. The maximum and minimum values of  $\gamma$  are 28,527.374 and 3,182.923  $\text{W}^{-1}\cdot\text{km}^{-1}$  when  $D$  is 16.07 and 64.28  $\mu\text{m}$ . In contrast, the minimum and maximum values of  $A_{\text{eff}}$  are 0.593 and 5.312  $\mu\text{m}^2$  when  $D$  is 16.07 and 64.28  $\mu\text{m}$ . We achieved much higher nonlinear coefficients and much smaller effective mode

areas than those in other works [22, 24, 32, 33] with  $\text{As}_2\text{S}_3$ -based suspended-core PCFs.

The very high values of the nonlinear coefficients and very small values of the effective mode area are the outstanding advantages of this work. This is favourable for us to propose optimal PCF structures and study SC generation in future publications.

**Table 2.** Values of nonlinear coefficients at 1.55  $\mu\text{m}$  wavelength of PCFs with various fiber diameters

| $D$ ( $\mu\text{m}$ ) | $\gamma$ ( $\text{W}^{-1}\cdot\text{km}^{-1}$ ) | $D$ ( $\mu\text{m}$ ) | $\gamma$ ( $\text{W}^{-1}\cdot\text{km}^{-1}$ ) | $D$ ( $\mu\text{m}$ ) | $\gamma$ ( $\text{W}^{-1}\cdot\text{km}^{-1}$ ) |
|-----------------------|---|-----------------------|---|-----------------------|---|
| 16.070                | 28527.374                                       | 32.140                | 10728.575                                       | 48.210                | 5496.674  |
| 17.677                | 25542.965                                       | 33.747                | 9900.805  | 49.817                | 5053.423  |
| 19.284                | 22902.698                                       | 35.354                | 9162.311  | 51.424                | 4774.345  |
| 20.891                | 20588.186                                       | 36.961                | 8501.258  | 53.031                | 4517.534  |
| 22.498                | 18566.324                                       | 38.568                | 7907.538  | 54.638                | 4280.721  |
| 24.105                | 16800.585                                       | 40.175                | 7372.577  | 56.245                | 4061.902  |
| 25.712                | 15256.294                                       | 41.782                | 6889.053  | 57.852                | 3859.321  |
| 27.319                | 13902.226                                       | 43.389                | 6450.766  | 59.459                | 3671.440  |
| 28.926                | 12711.121                                       | 44.996                | 6052.348  | 61.066                | 3496.862  |
| 30.533                | 11659.775                                       | 46.603                | 5689.220  | 62.673                | 3334.383  |
|                       |   |                       |   | 64.280                | 3182.923  |

**Table 3.** Values of effective mode area at 1.55  $\mu\text{m}$  wavelength of PCFs with various fiber diameters

| $D$ ( $\mu\text{m}$ ) | $A_{\text{eff}}$ ( $\mu\text{m}^2$ ) | $D$ ( $\mu\text{m}$ ) | $A_{\text{eff}}$ ( $\mu\text{m}^2$ ) | $D$ ( $\mu\text{m}$ ) | $A_{\text{eff}}$ ( $\mu\text{m}^2$ ) |
|-----------------------|--------------------------------------|-----------------------|--------------------------------------|-----------------------|--------------------------------------|
| 16.070                | 0.593                                | 32.140                | 1.576                                | 48.210                | 3.076                                |
| 17.677                | 0.662                                | 33.747                | 1.708                                | 49.817                | 3.346                                |
| 19.284                | 0.738                                | 35.354                | 1.845                                | 51.424                | 3.541                                |
| 20.891                | 0.821                                | 36.961                | 1.989                                | 53.031                | 3.743                                |
| 22.498                | 0.911                                | 38.568                | 2.138                                | 54.638                | 3.950                                |
| 24.105                | 1.006                                | 40.175                | 2.293                                | 56.245                | 4.163                                |
| 25.712                | 1.108                                | 41.782                | 2.454                                | 57.852                | 4.381                                |
| 27.319                | 1.216                                | 43.389                | 2.621                                | 59.459                | 4.605                                |
| 28.926                | 1.330                                | 44.996                | 2.794                                | 61.066                | 4.835                                |
| 30.533                | 1.450                                | 46.603                | 2.972                                | 62.673                | 5.071                                |
|                       |                                      |                       |                                      | 64.280                | 5.312                                |

### 3.4 Confinement loss

Confinement loss ( $L_c$ ), an important parameter for generating SC spectra in PCFs, is determined from the PCF structural parameters, such as air-hole diameters, lattice types and constants, and the refractive index of the air-hole-filled material. It can be derived from the imaginary part of the effective refractive index of the PCF according to Formula 5 [33]

$$L_c = 8.686 \frac{2\pi}{\lambda} \text{Im}[n_{\text{eff}}(\lambda)]. \quad (5)$$

The confinement loss characteristics of the fundamental mode for the fibers are denoted in Fig. 6. It can be seen that the confinement loss decreases with the increase in fiber diameters. The confinement loss increases in the 2.6–3.0  $\mu\text{m}$  wavelength region, which conforms to the change of absorption coefficients of  $\text{As}_2\text{S}_3$  in the long-wavelength region. A very low value of confinement loss was achieved, approximately at  $10^{-11}$   $\text{dB}\cdot\text{m}^{-1}$  for smaller fiber diameters. With the suspended-core structure of the designed PCFs, the modes are well confined in the core, and the electromagnetic field is primarily located there, resulting in a very low value of  $L_c$ . This is very beneficial for generating SC with a broadened spectrum. The very low values of  $L_c$  at the 1.55  $\mu\text{m}$  wavelength can be found for fibers with larger diameters (Table 4). The highest value of  $L_c$  is  $4.707 \times 10^{-11}$   $\text{dB}\cdot\text{m}^{-1}$  with a fiber diameter of 16.07  $\mu\text{m}$ . This  $L_c$  value is much lower than that of other publications [33], in which PCFs with selectively

air-hole filled  $\text{As}_2\text{S}_5$ - $\text{As}_2\text{S}_3$  hybrid was designed by numerical modelling.

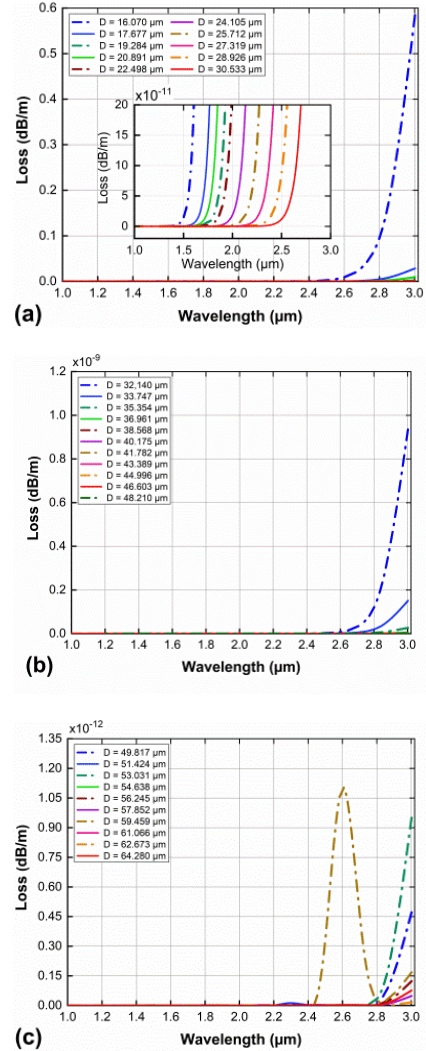


Fig. 6. Confinement loss of PCFs with various fiber diameters

Table 4. Values of confinement loss at 1.55  $\mu\text{m}$  wavelength of PCFs with various fiber diameters

| $D$ ( $\mu\text{m}$ ) | $L_c$ ( $\text{dB}\cdot\text{m}^{-1}$ ) | $D$ ( $\mu\text{m}$ ) | $L_c$ ( $\text{dB}\cdot\text{m}^{-1}$ ) | $D$ ( $\mu\text{m}$ ) | $L_c$ ( $\text{dB}\cdot\text{m}^{-1}$ ) |
|-----------------------|---|-----------------------|---|-----------------------|---|
| 16.070                | $4.707 \times 10^{-11}$                 | 32,140                | $-1.062 \times 10^{-15}$                | 48.210                | $6.050 \times 10^{-17}$                 |
| 17.677                | $1.315 \times 10^{-12}$                 | 33.747                | $-2.304 \times 10^{-15}$                | 49.817                | $-4.343 \times 10^{-16}$                |
| 19.284                | $5.424 \times 10^{-14}$                 | 35.354                | $-6.000 \times 10^{-17}$                | 51.424                | $-1.466 \times 10^{-16}$                |
| 20.891                | $3.039 \times 10^{-13}$                 | 36.961                | $-1.183 \times 10^{-15}$                | 53.031                | $1.314 \times 10^{-16}$                 |
| 22.498                | $2.184 \times 10^{-14}$                 | 38.568                | $1.260 \times 10^{-16}$                 | 54.638                | $-4.913 \times 10^{-16}$                |



| $D$ ( $\mu\text{m}$ ) | $L_c$ ( $\text{dB}\cdot\text{m}^{-1}$ ) | $D$ ( $\mu\text{m}$ ) | $L_c$ ( $\text{dB}\cdot\text{m}^{-1}$ ) | $D$ ( $\mu\text{m}$ ) | $L_c$ ( $\text{dB}\cdot\text{m}^{-1}$ ) |
|-----------------------|---|-----------------------|---|-----------------------|---|
| 24.105                | $1.235\times 10^{-15}$                  | 40.175                | $6.290\times 10^{-16}$                  | 56.245                | $-3.855\times 10^{-17}$                 |
| 25.712                | $2.349\times 10^{-16}$                  | 41.782                | $-3.730\times 10^{-15}$                 | 57.852                | $-6.002\times 10^{-16}$                 |
| 27.319                | $-1.800\times 10^{-17}$                 | 43.389                | $7.670\times 10^{-16}$                  | 59.459                | $3.799\times 10^{-17}$                  |
| 28.926                | $-6.052\times 10^{-16}$                 | 44.996                | $1.554\times 10^{-15}$                  | 61.066                | $-1.446\times 10^{-18}$                 |
| 30.533                | $-2.081\times 10^{-16}$                 | 46.603                | $-7.035\times 10^{-16}$                 | 62.673                | $5.511\times 10^{-17}$                  |
|                       |   |                       |   | 64.280                | $5.288\times 10^{-17}$                  |

### 3.5 Optimization of structural parameters of PCFs for SC generation

The optical pulse per unit distance of the propagation length of the fiber is changed by chromatic dispersion, so a PCF with suitable dispersion properties is a crucial condition dominating the efficiency of SC generation. The low anomalous dispersion near the ZDW, consisting of one ZDW and two ZDWs, provides the generation of a broad supercontinuum with strong confinement to the core despite low input power through soliton effects. Furthermore, the nonlinear properties, such as nonlinear coefficients, effective mode area, and confinement loss, contribute to generating new frequencies through the interaction of the input pulses with nonlinear media, such as PCFs. For that reason, two PCFs were proposed to consider for SC generation that must satisfy the above optical properties. Based on the above results, we introduce two structures, with  $D$  being 16.07 and 64.28  $\mu\text{m}$ , which have flat anomalous dispersion, high nonlinear coefficients, and low confinement loss. Those two structures are named #F<sub>1</sub> and #F<sub>2</sub>, with the lattice parameters shown in Table 5.

Fig. 7 shows the optical properties of the selected PCFs, where the optical properties of the

#F<sub>1</sub> and #F<sub>2</sub> fibers are assigned blue and red. Both fibers exhibit anomalous dispersion properties. The #F<sub>1</sub> fiber with a smaller core diameter has two ZDWs, with a recommended pump wavelength of 1.55  $\mu\text{m}$ , which is a practical common pumping wavelength of the laser, near the maximum value of dispersion. In contrast, the #F<sub>2</sub> fiber with a larger core diameter possesses flat anomalous dispersion, with one ZDW and has an expected pumping wavelength of 2.28  $\mu\text{m}$  (Fig. 7a). In the studied wavelength region, the #F<sub>2</sub> fiber has a smaller dispersion value, but its effective mode area is larger than that of the #F<sub>1</sub> fiber because of its large core, which means that the #F<sub>1</sub> fiber gets a higher nonlinearity coefficient. The confinement loss of the #F<sub>1</sub> fiber is also higher than that of the #F<sub>2</sub> fiber (Figs. 7b and 7c). Note that we have a priority to control how the structure is designed to suit the application purpose since the optical properties of PCFs are difficult to optimize simultaneously. In this paper, both selected PCFs are suitable for SC generation because of their advantages according to each separate optical property. The nonlinear characteristic values at the pump wavelength are introduced in Table 6 in comparison with those of some previous publications on As<sub>2</sub>S<sub>3</sub>-based PCFs.

Table 5. Lattice parameters of two proposed PCFs

| #               | $D$ ( $\mu\text{m}$ ) | $R_{\text{hole}}$ ( $\mu\text{m}$ ) | $r_c$ ( $\mu\text{m}$ ) | $t_c$ ( $\mu\text{m}$ ) |
|-----------------|-----------------------|-------------------------------------|-------------------------|-------------------------|
| #F <sub>1</sub> | 16.07                 | 7.615                               | 0.41                    | 0.125                   |
| #F <sub>2</sub> | 64.28                 | 30.46                               | 1.64                    | 0.5                     |

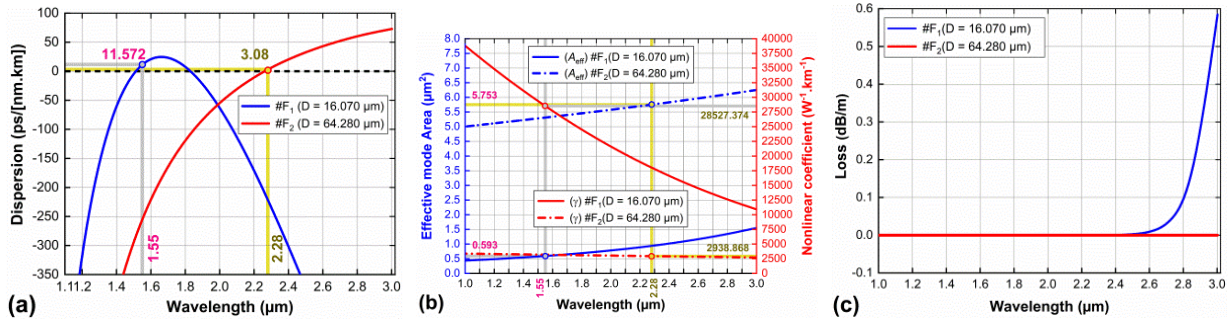


Fig. 7. Optical properties of the proposed PCFs with various fiber diameter (a) chromatic dispersion, (b) nonlinear coefficient and effective mode area, and (c) confinement loss

Table 6. Comparison of nonlinear characteristic values at pump wavelength of proposed PCFs with some previous publications on As<sub>2</sub>S<sub>3</sub>-based PCFs

| #  | Refs.,<br>Year   | D<br>(μm) | Pump<br>wavelength<br>(μm) | D <sub>c</sub><br>(ps·nm·km <sup>-1</sup> ) | γ<br>(W <sup>-1</sup> ·km <sup>-1</sup> ) | A <sub>eff</sub><br>(μm <sup>2</sup> ) | L <sub>c</sub><br>(dB·m <sup>-1</sup> ) |
|--|------------------|-----------|----------------------------|---|---|--|---|
| #F <sub>1</sub> (this work)  |                  | 16.070    | 1.55                       | 11.572                                      | 28527.374                                 | 0.593                                  | 4.707×10 <sup>-11</sup>                 |
| #F <sub>2</sub> (this work)  |                  | 64.280    | 2.28                       | 3.08  | 2938.868                                  | 5.753                                  | 4.615×10 <sup>-16</sup>                 |
| PCF with<br>suspended core<br>As <sub>2</sub> S <sub>3</sub>                 | Weiqing,<br>2013 | 160       | 2.5                        | –   | 894.2                                     | 8.43                                   | 1.0                                     |
| PCF with<br>suspended core<br>As <sub>2</sub> S <sub>3</sub>                 | Nian,<br>2018    | 5.0       | 2.0                        | 14.19                                       | 561                                       | 18.4                                   | 5.7                                     |
| Suspended core<br>As <sub>2</sub> S <sub>3</sub> tapered<br>fiber            | Imtiaz,<br>2020  | 11.5      | 1.938                      | –8.32                                       | 3210                                      | –                                      | –                                       |
| As <sub>2</sub> S <sub>5</sub> -As <sub>2</sub> S <sub>3</sub><br>hybrid PCF | Chen,<br>2017    | –         | 4.5                        | 0.025                                       | 104                                       | 25.7                                   | 3.7×10 <sup>-7</sup>                    |

## 4 Conclusion

In this paper, we reported on the optical properties of As<sub>2</sub>S<sub>3</sub>-based suspended-core photonic crystal fibers with changing lattice parameters. The anomalous dispersion with two zero-dispersion wavelengths, a very high nonlinear coefficient, a small effective mode area, and a low confinement loss in comparison with previous works are the highlights of our work. Two structures with optimal properties were

proposed and analyzed in detail to show their outstanding advantages in SC generation orientation.

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